

# **HCCI Combustion: the Sources of Emissions at Low Loads and the Effects of GDI Fuel Injection**

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# Introduction

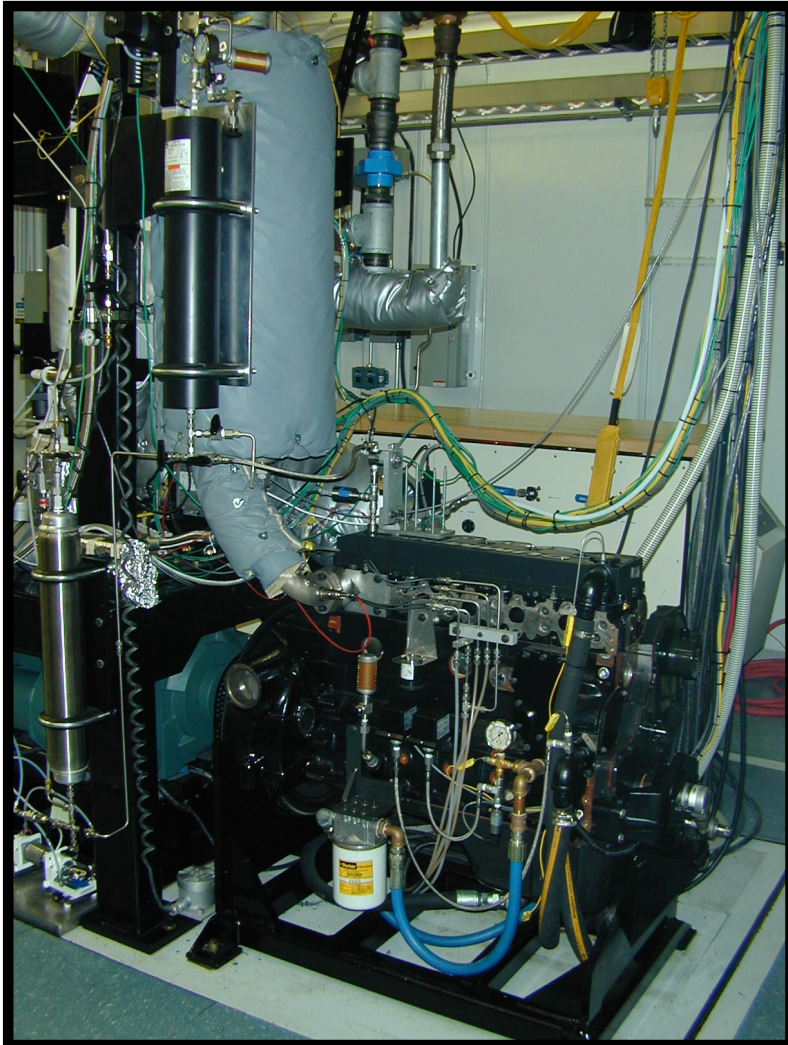
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- HCCI engines are a low-emissions alternative to diesel engines.
  - Provide diesel-like or higher efficiencies.
  - Very low engine-out  $\text{NO}_x$  and PM emissions.
- Research is required in many areas to resolve technical barriers to the development of HCCI engines by industry.
  - The objective of our work is to help provide this understanding.
- Establish a laboratory to investigate HCCI combustion fundamentals.
  - All-metal engine: fully operational – result are subject of presentation.
  - Optically accessible engine: examine in-cylinder processes (end of 02).
- CHEMKIN kinetic-rate computations
  - Guide experiments
  - Assist in data analysis
  - Show limiting behavior

# Engine and Operating Conditions



## *HCCI All-Metal Engine*



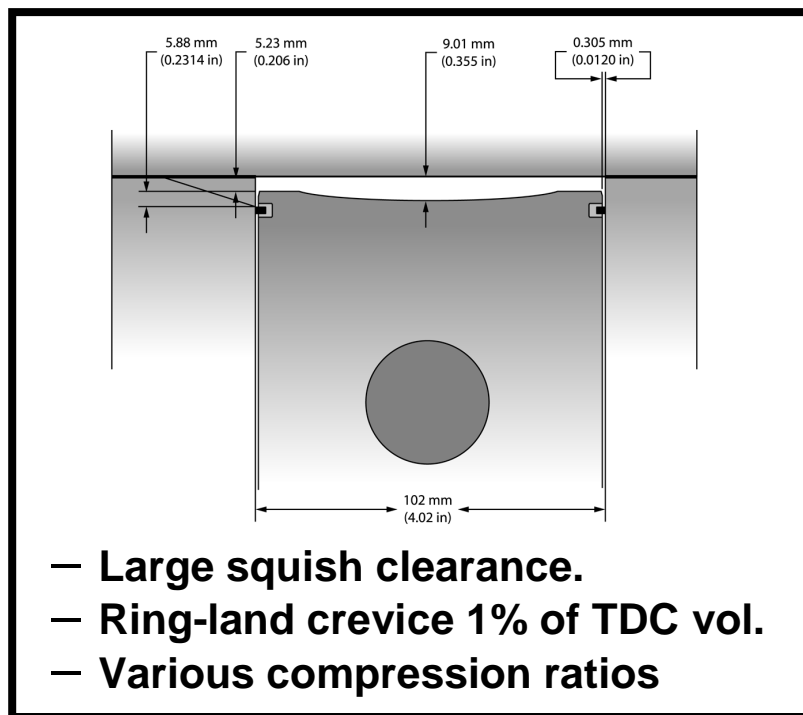
Based on Cummins B, 0.98 ltr./cyl.

- Six-cylinder diesel engine converted for balanced, single-cyl., HCCI operation.
- Versatile facility to investigate various operational and control strategies.
  - Compression ratios from 13 - 21 **(18)\***
  - Swirl ratios from 0.9 - 3.2; 7.2 **(0.9)\***
  - Speeds to 3600 rpm **(600 - 1800 rpm)\***
  - Multiple fueling systems.
    - > Fully premixed **(curr.)\***
    - > Port fuel injection (PFI)
    - > Direct injection, gasoline-type **(curr.)\***
    - > Direct injection, diesel-type
  - Liquid or gas-phase fuels **(iso-octane)\***
- Complete intake charge conditioning.
  - Intake temperatures to 180° C. **(varies)\***
  - Intake pressures to 4 bars. **(varies)\***
  - Simulated or real EGR. **(none)\***

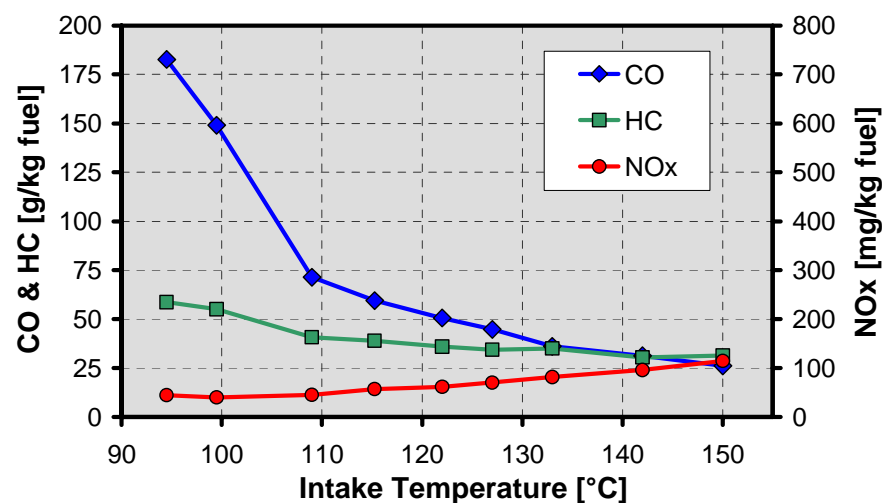
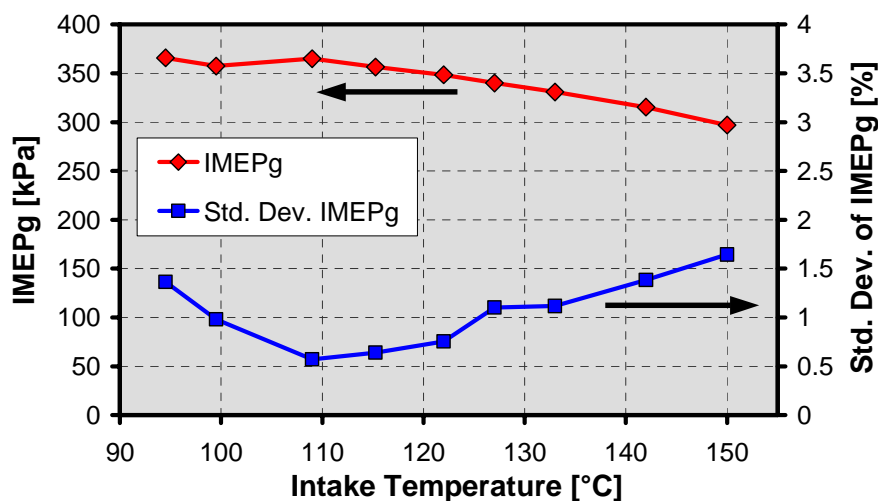
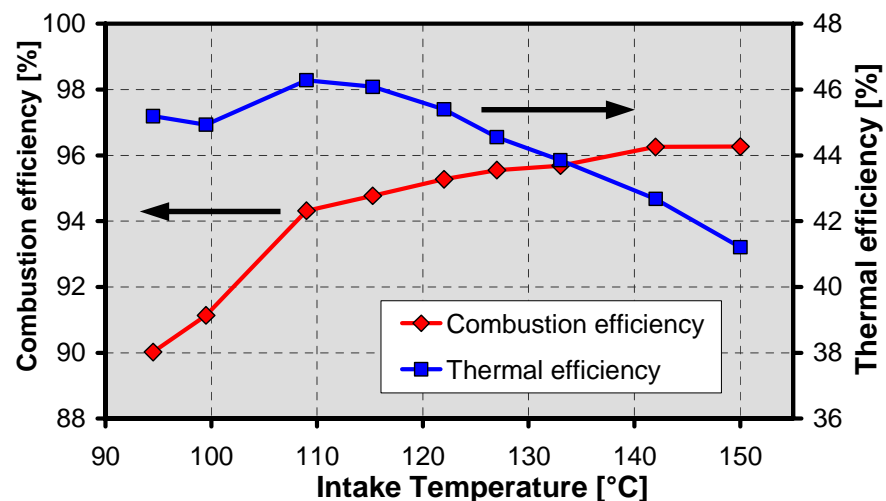
\* Values in **(red)** are used for current work.



# Engine Appears to be Working Well



$CR = 18; \phi = 0.24; P_{in} = 120 \text{ kPa};$   
 $1200 \text{ rpm}; \text{Well-Mixed Charge}$





# Computational Approach

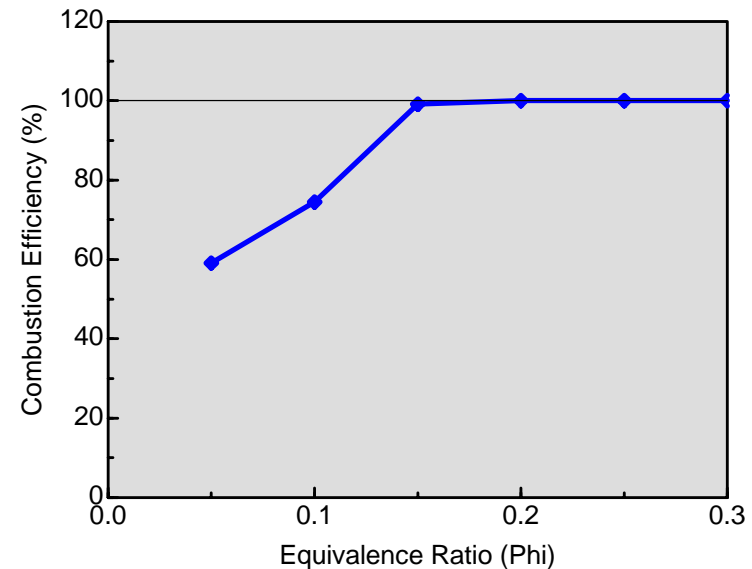
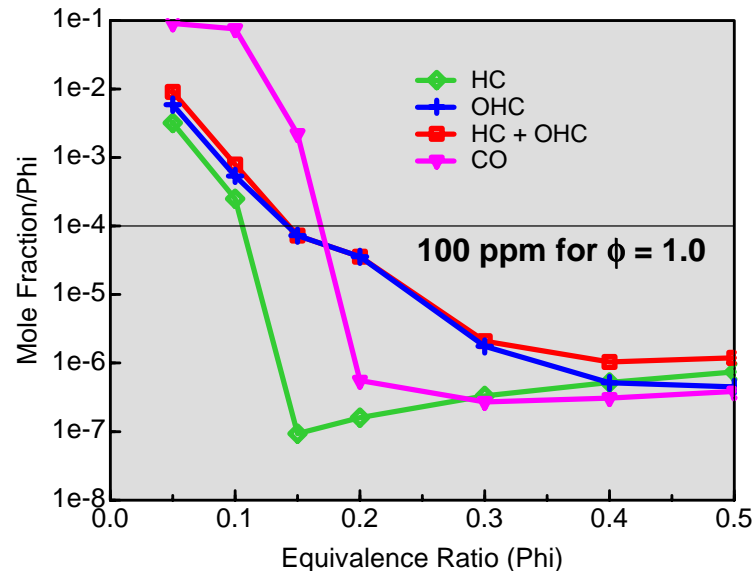
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- Senkin application of the CHEMKIN-III kinetics rate code.
  - Single-zone model with uniform properties and no heat transfer.
  - Allows compression and expansion with slider-crank relationship.
  - Full chemistry for iso-octane (Westbrook *et al.*, LLNL).
- Great oversimplification of a real engine. Model cannot reproduce all real-engine behavior.
- Model is well suited for investigating certain fundamental aspects of HCCI combustion.
  - Allows the effects of kinetics and thermodynamics to be isolated and evaluated without complexities of walls, crevices, and inhomogeneities.
    - > Assists in analysis of experimental data by separating chemical-kinetic and physical effects.
  - Represents the adiabatic limit for bulk-gas behavior in real engines.
  - Guide experiments by showing approximate trends in ignition timing & temperature compensation with changes in operating conditions.

# CHEMKIN predicts incomplete bulk-gas reactions at low loads.



Iso-Octane; 1800 rpm; CR = 21;  $T_{in} = 380$  K;  $P_{in} = 1$  atm.

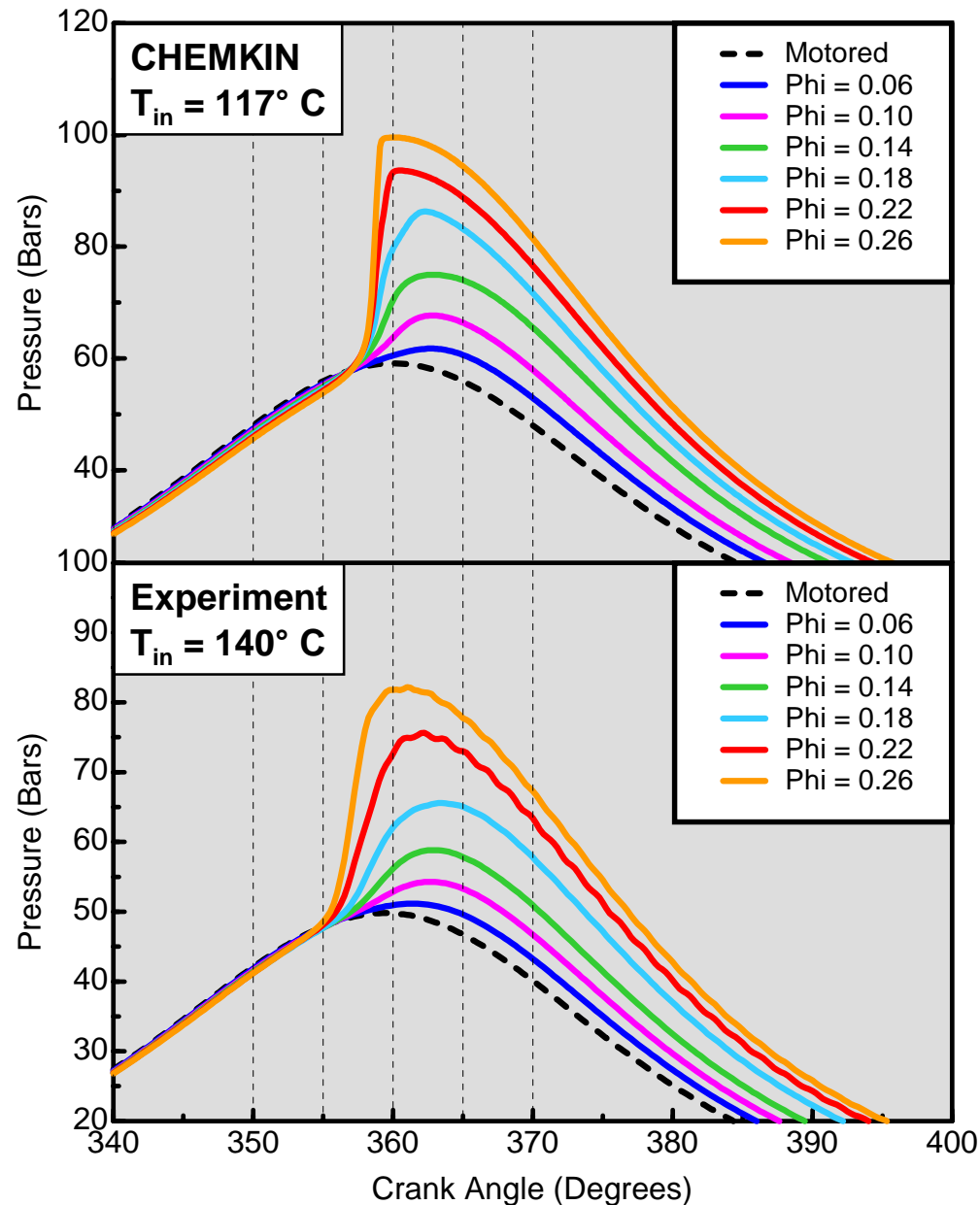


- Below  $\phi = 0.2$ , emissions rise followed by a drop in combustion efficiency.
  - Temperatures are too low to complete reactions, especially  $\text{CO} \rightarrow \text{CO}_2$ .
- Indicates high emissions of OHC as well as CO and HC.
  - OHC not well-detected by standard FID HC detector, and they can be harmful.
- Results for bulk-gas alone, in the absence of heat transfer.
  - Occurs in range of interest (typical diesel idle conditions are  $\phi = 0.10 - 0.12$ ).
  - In real engine, heat transfer will shift onset of incomplete reactions to higher  $\phi$ .
  - Walls & crevices also add to emissions.

**SAE Paper 2002-01-1309**



# Vary $\phi$ : Experiment and CHEMKIN

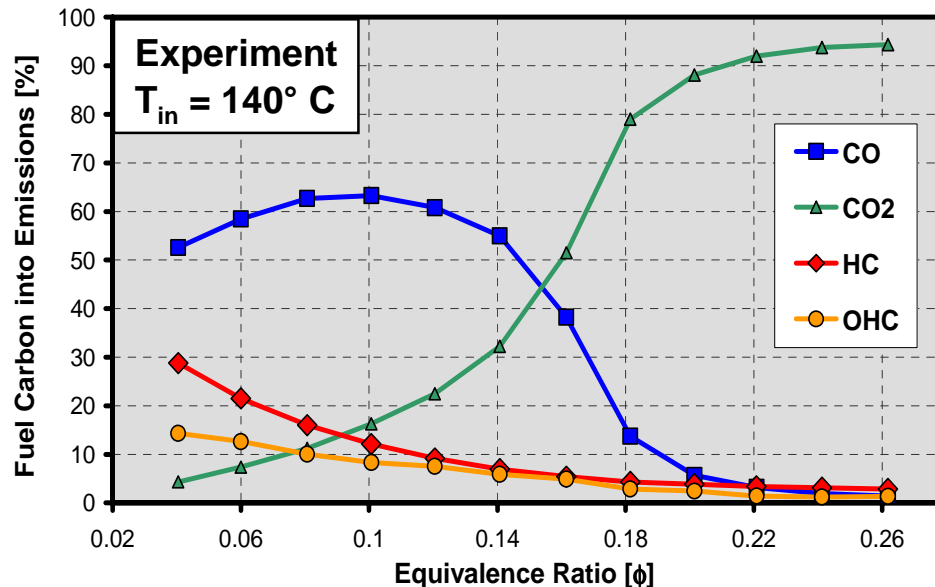
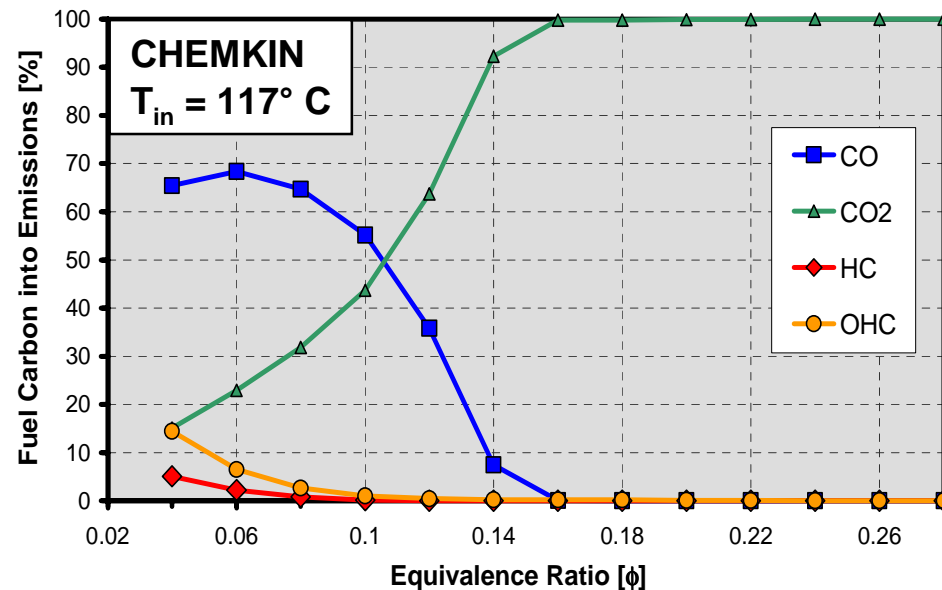


***Iso-Octane ; CR = 18; 1200 rpm;  
 $P_{in} = 120 \text{ kPa}$ ; Pre-Mixed***

- Intake temperature adjusted for 50% burn at TDC for  $\phi = 0.14$ .
  - Experiment:  $T_{in} = 140^\circ \text{ C}$
  - CHEMKIN:  $T_{in} = 117^\circ \text{ C}$
- Experiment shows greater variation in combustion phasing.
  - Heat transfer and residuals.
  - Advanced timing at higher loads has little effect on emissions.
  - Timing retard at low loads is small and has little effect on emissions.



# Emissions: Experiment and CHEMKIN

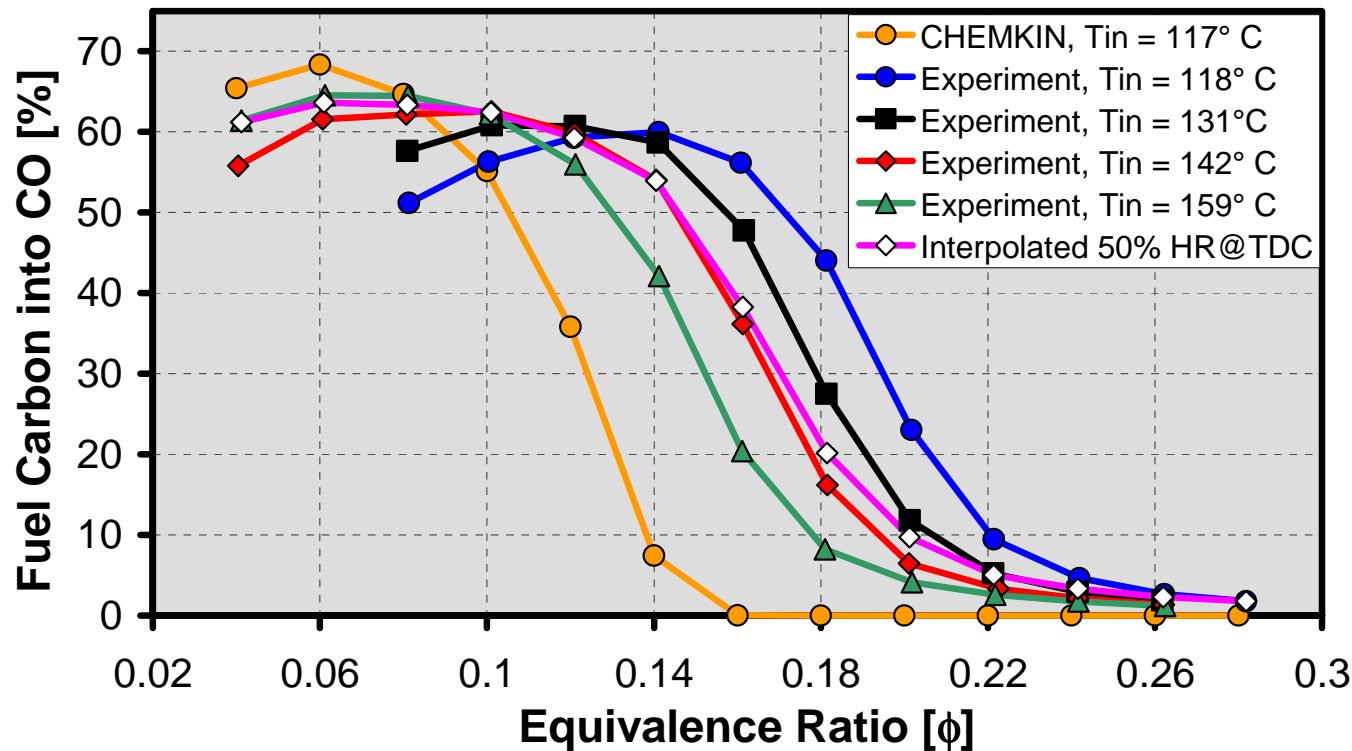


**1200 rpm;  $CR = 18$ ;  $P_{in} = 120 \text{ kPa}$ ;  
Pre-Mixed Fueling**

- Experimental  $T_{in}$  was increased to maintain near-TDC ignition.
  - Compensate for heat transfer.
- Experimental emissions match model closely.
  - CO levels match closely ~65% > Bulk-gas source.
  - HC, rise for  $\phi < 0.2$  is similar to model indicates bulk-gas source at low  $\phi$ .
    - > Near-constant baseline level for  $\phi > 0.2$  suggest crevice source.
  - “Missing carbon” in experiment indicates presence of OHCs.
    - > Similar to model, but lower due to FID response.



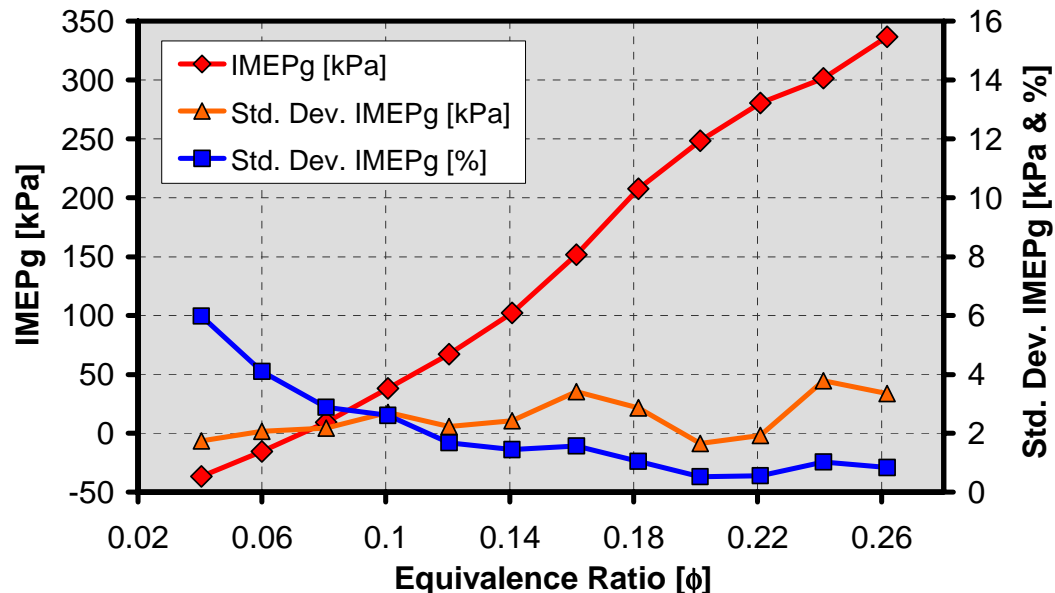
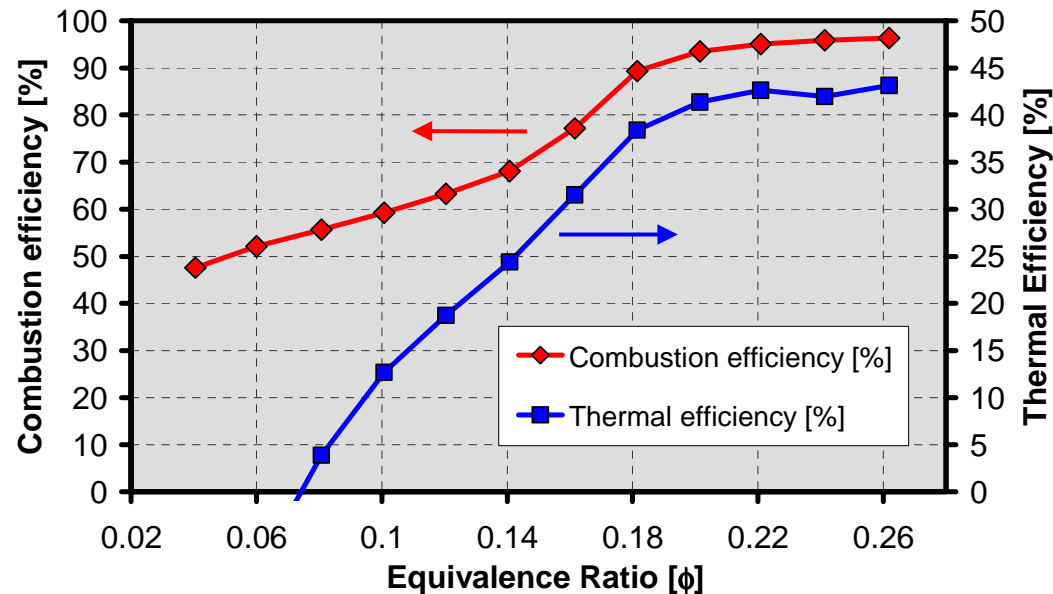
# Comparison of CO Emissions with $\phi$ at Various $T_{in}$



- Magnitude of increase in CO with decreasing  $\phi$  agrees well with the CHEMKIN results. Shows incomplete bulk-gas reactions are the cause.
  - Onset of rise in CO levels is shifted to higher  $\phi$  in engine due to heat transfer.
  - Rise in CO shifts to progressively higher  $\phi$  as  $T_{in}$  is reduced (lower  $T_{\text{combustion}}$ ).
  - Engine data also show a large drop in combustion efficiency at low loads, corresponding to the increase in CO.



# Efficiencies and Combustion Stability

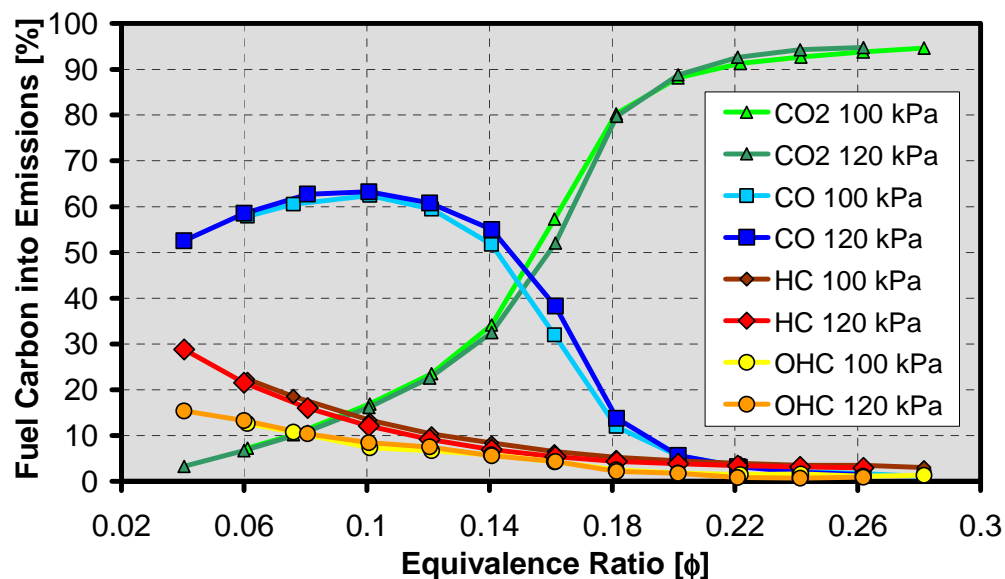


**$CR = 18$ ;  $P_{in} = 120 \text{ kPa}$ ;  
 $T_{in} = 140^\circ \text{ C}$ ; Pre-Mixed**

- Combustion efficiency drops from 95% to 60% as fuel is reduced to low-idle,  $\phi = 0.1$ .
  - Similar drop in pressure-indicated thermal efficiency.
  - Commensurate with the rapid rise in CO.
- Std. Dev. of IMEP is 2 – 4 kPa for all fueling rates ( $\phi$ ).
  - Increase at  $\phi = 0.16$  due to this being in the middle of the rapid rise in CO.
- Normalized  $\sigma$ IMEP increases below  $\phi = 0.1$  because IMEP is near zero.
  - Std. Dev. of IMEPg  $\leq 2.6\%$  from  $\phi = 0.1$  to  $\phi = 0.26$ .

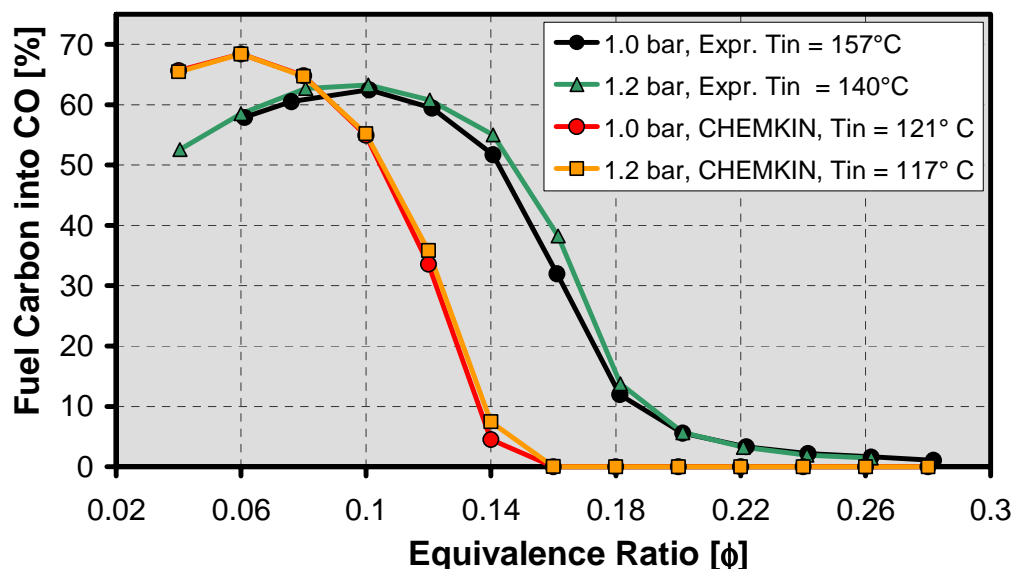


# Effect of Intake Pressure

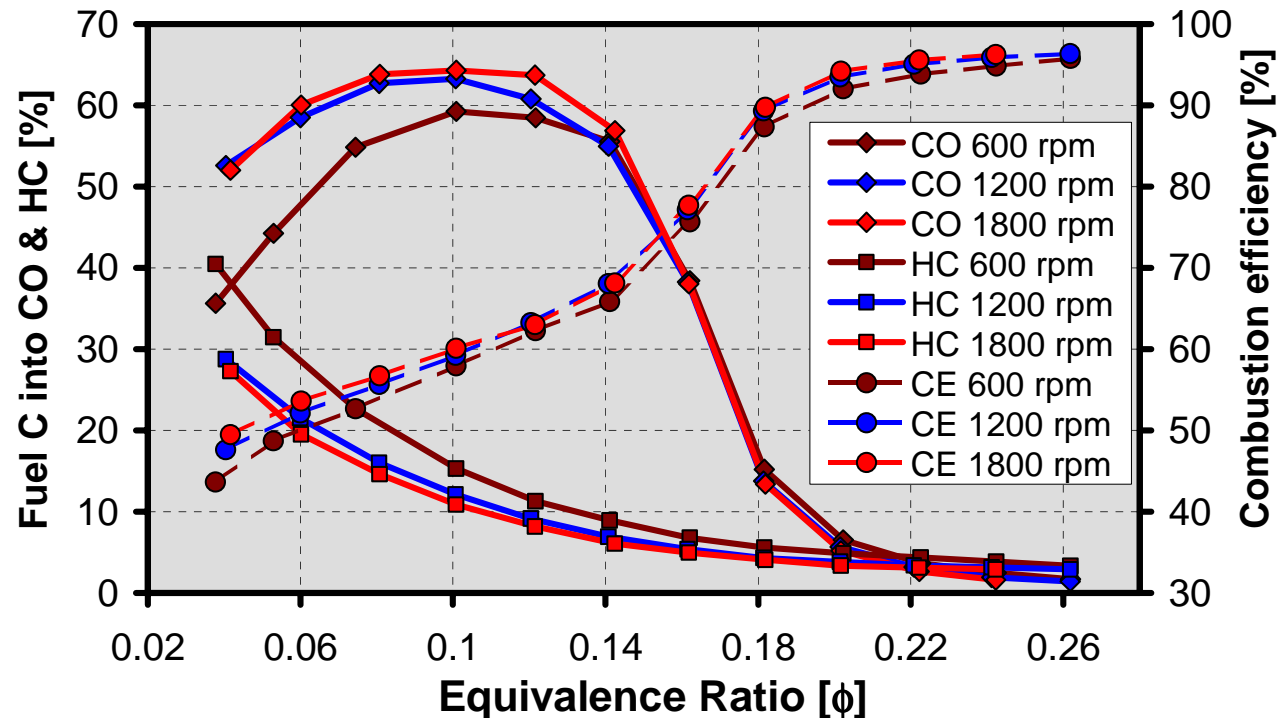


**1200 rpm; CR = 18; Pre-Mixed**

- Changing  $P_{in}$  from 101 to 120 kPa has little effect on onset of incomplete bulk-gas reactions when combustion phasing is maintained.
  - Experiment and CHEMKIN both show slightly lower CO values during rapid rise.
- $T_{in}$  adjusted for 50% burn at TDC for  $\phi = 0.14$ .
  - 101 kPa:  $T_{in} = 157^\circ \text{C}$
  - 120 kPa:  $T_{in} = 140^\circ \text{C}$

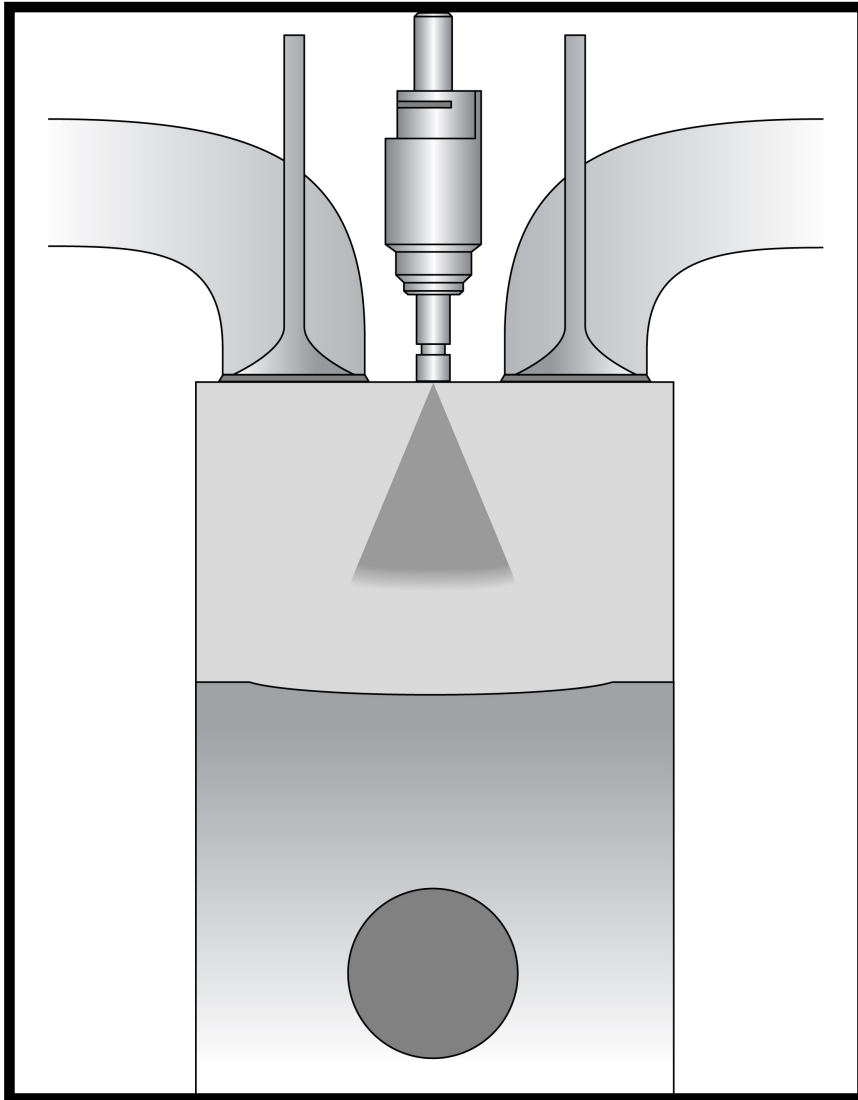


# Effect of Engine Speed on Bulk-Gas Reactions



- $T_{in}$  adjusted to maintain combustion phasing at TDC for  $\phi = 0.14$ .
  - Higher compression temperatures compensate for reduced time for reactions.
- Engine speed has little effect on the fueling rate at which the onset of incomplete bulk-gas reactions occurs – for iso-octane.
  - In agreement with CHEMKIN computations.
- Results suggest that special combustion strategies will be required for low-load operation.

# GDI Fueling: Vary Injection Timing



## Early Injection

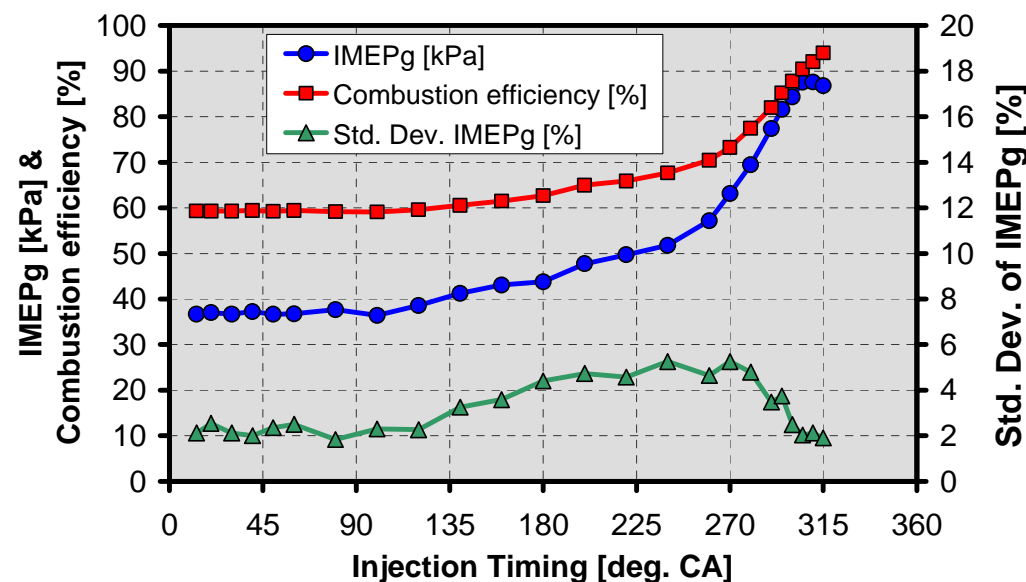
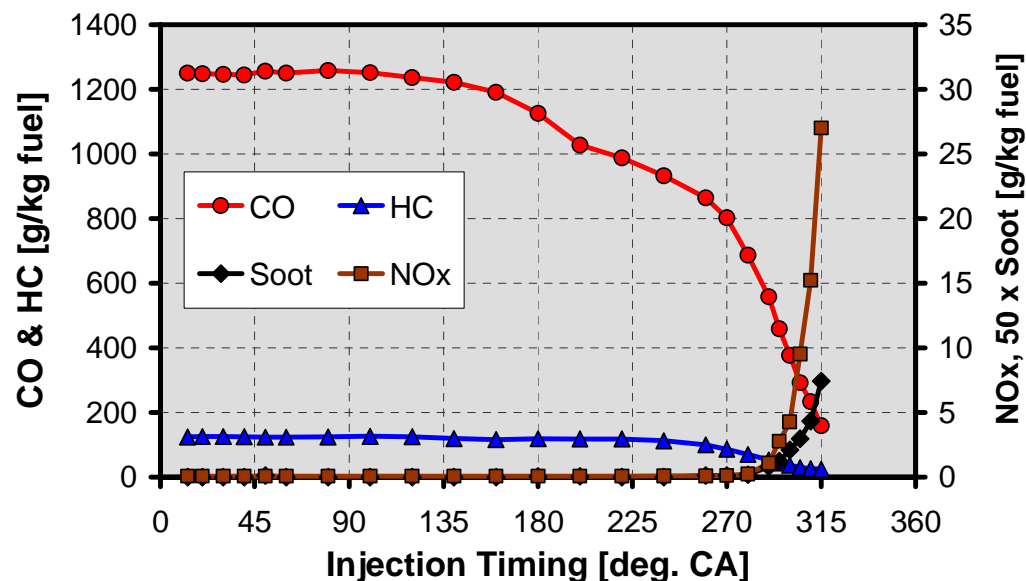
- Provides a fairly uniform mixture.
  - Can lead to incomplete bulk-gas reactions at low loads, as predicted by CHEMKIN.

## Late Injection

- Can provide partial charge stratification.
  - Mixture locally richer for the same fueling rate.
  - Offers the potential to mitigate incomplete bulk-gas reactions at light loads.
- Also, could prevent fuel from reaching ring-land crevice.
  - Reduce baseline emissions.



# Variation in Injection Timing: $\phi = 0.1$



$T_{in} = 142^{\circ} \text{C}$ ;  $P_{in} = 120 \text{ kPa}$ ;  
1200 rpm; GDI fueling

- Early injection (0-90° aTDC intake) provides a well-mixed charge.
  - High CO and low combustion efficiency for  $\phi = 0.1$ .
- Retarding injection improves combustion and emissions for low-load operation.
  - Injection at 290° reduces CO and HC emission substantially with only about 1g/kg-fuel  $\text{NO}_x$  (4 ppm).
  - Combustion efficiency increases from 59% to 82%.
- Further improvements possible with optimized stratification.

# Summary and Conclusions - 1



- Metal HCCI research engine appears to be functioning well.
  - At fully combusting conditions:  $\eta_{\text{thermal}} \sim 46\%$ ,  $\sigma\text{IMEP} < 1\%$ ,  $\text{CO} < 65 \text{ g/kg (1000 ppm)}$ ,  $\text{HC} < 35 \text{ g/kg (1200 ppm)}$ ,  $\text{NO}_x \sim 0.06 \text{ g/kg (1 ppm)}$ .
- CHEMKIN results show that for fuel loads below  $\phi \sim 0.16$ , bulk-gas reactions are incomplete, even for an idealized adiabatic engine.
  - Significant combustion inefficiencies, very high CO, and increased HC.
    - > Temperatures are too low to complete reactions, mainly  $\text{CO} \rightarrow \text{CO}_2$ .
  - Indicate that significant OHC emissions should occur. (OHC is  $\sim 2\text{x HC}$ ).
- Experimental data show a very similar trend to the changes in emissions and combustion efficiency as fuel loading is reduced.
  - CO levels match very closely with those of the model ( $\sim 65\%$  of fuel C).
    - > Bulk-gas must be the source.
  - Onset of incomplete bulk-gas reactions occurs at higher  $\phi \sim 0.2$  due to heat transfer cooling the charge.





## Summary and Conclusions - 2

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- The “missing carbon” in the emissions measurements matches the expected OHC trends.
  - HC detector (FID) has low sensitivity to OHC.
- Combustion stability was good even at idle loads,  $\sigma\text{IMEP} \leq 2.6\%$ .
- Increasing  $P_{\text{in}}$  from 1.0 to 1.2 bars had little effect on the onset or magnitude of incomplete bulk-gas reactions when ignition timing was maintained.
- Changing speed from 600 to 1800 rpm has almost no effect on the onset or magnitude of incomplete bulk-gas reactions for iso-octane.
  - Increased compression temperatures required to maintain ignition timing compensate for reduced time to complete reactions.
- Partial charge stratification by late-cycle fuel injection appears to have a strong potential for mitigating the difficulties of low-load operation.